High-voltage vertical Ga$_2$O$_3$ power rectifiers operational at high temperatures up to 600 K

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ABSTRACT
This work presents the temperature-dependent forward conduction and reverse blocking characteristics of a high-voltage vertical Ga$_2$O$_3$ power rectifier from 300 K to 600 K. Vertical β-Ga$_2$O$_3$ Schottky barrier diodes (SBDs) were fabricated with a bevel-field-plated edge termination, where a beveled sidewall was implemented in both the mesa and the field plate oxide. The Schottky barrier height was found to increase from 1.2 eV to 1.3 eV as the temperature increases from 300 K to 600 K, indicating the existence of barrier height inhomogeneity. The net donor concentration in the drift region shows little dependence on the temperature. The reverse leakage current up to 500 V was found to be limited by both the thermionic-field electron injection at the Schottky contact and the electron hopping via the defect states in the depletion region. At 300–500 K, the leakage is first limited by the electron injection at low voltages and then by the hopping in depleted Ga$_2$O$_3$ at high voltages. At temperatures above 500 K, the thermionic field emission limits the device leakage over the entire voltage range up to 500 V. Compared to the state-of-the-art SiC and GaN SBDs when blocking a similar voltage, our vertical Ga$_2$O$_3$ SBDs are capable of operating at significantly higher temperatures and show a smaller leakage current increase with temperature. This shows the great potential of Ga$_2$O$_3$ SBDs for high-temperature and high-voltage power applications.

Ultra-wide-bandgap semiconductor gallium oxide (Ga$_2$O$_3$) has emerged as a promising material for next-generation power electronics, due to its high critical electrical field ($E_c$), controllable doping, and the availability of large-diameter wafers. Recently, an $E_c$ over 5 MV/cm (Ref. 4) and an electron mobility of 176 cm$^2$/Vs (Ref. 5) have been experimentally demonstrated in Ga$_2$O$_3$, making Ga$_2$O$_3$ particularly attractive for medium- and high-voltage (>600 V) power devices. A breakdown voltage (BV) over 600 V has been demonstrated in a variety of Ga$_2$O$_3$ power devices, including lateral MOSFETs, lateral Schottky barrier diodes (SBDs), vertical power FinFETs, and vertical SBDs.

While the room-temperature performance of Ga$_2$O$_3$ power devices, i.e., the trade-off between the on-resistance ($R_{on}$) and BV, is still inferior to that of the state-of-the-art SiC and GaN devices, Ga$_2$O$_3$ devices have shown great promise for high-temperature applications. With an ultrawide bandgap of 4.8 eV, the intrinsic carrier density in Ga$_2$O$_3$ is significantly lower than that in Si, SiC, and GaN, allowing Ga$_2$O$_3$ to maintain effective doping up to very high temperatures. Before the availability of single-crystalline Ga$_2$O$_3$ wafers, polycrystalline Ga$_2$O$_3$ has long been used for making high-temperature gas sensors with an operating temperature up to 1000 °C. In addition, thermally stable Schottky barrier contacts have been recently demonstrated for Ga$_2$O$_3$ devices with an operating temperature up to 500 °C.

However, the majority of previous high-temperature studies on Ga$_2$O$_3$ devices have only focused on their forward characteristics. For example, high-temperature forward operations have been demonstrated in lateral Ga$_2$O$_3$ MOSFETs and vertical Ga$_2$O$_3$ SBDs up to 300 °C (Ref. 18) and 500 °C, respectively, whereas very few high-temperature demonstrations have been reported on the high-voltage blocking capability of Ga$_2$O$_3$ power devices. Higashiwaki et al. and Konishi et al. demonstrated the blocking characteristics of vertical Ga$_2$O$_3$ power diodes up to 200 V at 200 °C, which is the highest blocking
voltage that has been reported in Ga2O3 devices for high-temperature operation. This blocking voltage is much lower than the requirement for medium- and high-voltage power applications, indicating that the high-temperature blocking capability of Ga2O3 power devices has become a key roadblock for their applications in harsh-environment power systems (e.g., oil drilling, aerospace, etc.). From the viewpoint of device design, this issue could be attributed to the lack of a robust edge termination for Ga2O3 power devices, as the crowded electric field (E-field) at the device periphery often leads to a fast leakage increase at high voltages and high temperatures. On the other hand, very little is known about the high-temperature, high-voltage leakage mechanisms in Ga2O3 power devices.

In this work, we demonstrate a bevel-field-plated vertical Ga2O3 Schottky barrier diode (SBD) operational up to 600 K in both forward conduction and reverse high-voltage (>500 V). Two competing leakage mechanisms were unveiled, one being limited by Schottky barrier contact and dominating the low-voltage leakage behaviors while the other is limited by the depletion region and dominates the high-voltage leakage behaviors. The relation between these two mechanisms at different temperatures has also been systematically analyzed.

The schematic of the vertical Ga2O3 SBD fabricated in this work is shown in Figs. 1(a) and 1(b). Compared to the previously demonstrated bevel-field-plated Ga2O3 SBDs with only beveled mesas,22 our device also has a beveled sidewall at the field oxide in the vicinity of the Schottky contact, which could spread the crowded E-field at the contact edge.23 The epitaxial structure consists of a 11-μm thick Si-doped n-Ga2O3 layer grown by halide vapor phase epitaxy on a 2-in. Sn-doped n+Ga2O3 (001) substrate. The net donor concentration (ND - NA) in the n-Ga2O3 drift region was revealed to be ~1.5 × 10^16 cm^-3 based on C-V measurements. The device fabrication process is shown in Fig. 1(c). The spin-on-glass (SOG) was first deposited, followed by a patterned wet etch in 4% diluted HF to form the hard mask for mesa etching. The isotropic wet etch forms a ~45° angle at the SOG sidewall. ~1 μm Ga2O3 mesa etch was then performed in an Inductively Coupled Plasma—Reactive Ion Etching (ICP-RIE) system using BCl3 gas. Next, 650-nm thick SOG was deposited again as the field plate (FP) oxide. A blanket backside Ohmic contact was formed by a Ti/Au (30/150 nm) deposition followed by a 470 °C annealing in N2. The SOG was opened through wet etch and the Ni/Au stack was deposited for the Schottky and the FP metals. Finally, annealing at 350 °C in N2 was performed. As shown in Fig. 1(d), the fabricated device shows a ~45° beveled angle in both the Ga2O3 mesa and the SOG FPs. The circular anode diameter is 200–250 μm.

Figure 2(a) shows the forward current-voltage (I-V) characteristics of the fabricated Ga2O3 SBDs at the temperature (T) from 300 K to 600 K in a semilog plot. (b) Dependence of the Schottky barrier height, built-in potential, and ideality factor as a function of T extracted from the forward I-V-T characteristics. (c) Dependence of the built-in potential and the net donor concentration in the drift region as a function of T extracted from C-V-T characteristics. (d) Forward I-V characteristics in a linear plot. (e) The extracted differential Rsh at T of 300–600 K.
to 600 K. The forward $I$-$V$-$T$ characteristics can be well fitted by the thermionic emission (TE) model:\textsuperscript{15,20,21}

$$I = J_0 \exp \left( \frac{q(V - JR_0)}{n k T} \right) = A^* T^2 \exp \left( -\frac{q \varphi_b}{k T} \right) \exp \left( \frac{q(V - JR_0)}{n k T} \right),$$

(1)

where $J$, $J_0$, $k$, $R_0$, and $A^*$ are the current density, saturation current density, Boltzmann constant, series resistance, and effective Richardson constant, respectively. $A^*$ is used as 41 A/(cm$^2$ K$^2$) for Ga$_2$O$_3$ in this work.\textsuperscript{20,21} The Schottky barrier height ($\varphi_b$) and ideality factor ($n$) can be obtained by fitting the $\ln(J)$ vs $V$ in the linear range of the semilog plot.\textsuperscript{21} With the extracted $\varphi_b$, the built-in potential ($V_{bi}$) is given by\textsuperscript{20}

$$q V_{bi} = q \varphi_b - (E_C - E_f) = q \varphi_b - kT \ln \left( \frac{N_C}{N_D - N_A} \right),$$

(2)

where $N_C$ is the effective density of states in the conduction band of Ga$_2$O$_3$, which can be calculated as a function of $T$.\textsuperscript{22,23} Figure 2(b) shows the extracted $q \varphi_b$ vs $V_{bi}$ and $n$ of the fabricated vertical Ga$_2$O$_3$ SBDs at different $T$. $q \varphi_b$ increases from $\sim$1.2 eV at 300 K to $\sim$1.3 eV at 600 K. $n$ increases from 1.08 to 1.21 from 300 K to 600 K. This phenomenon can be attributed to the Schottky barrier height inhomogeneity that has been commonly observed in Ga$_2$O$_3$,\textsuperscript{21,23} and GaN SBDs. At low $T$, electrons preferentially flow through the lower barriers. As $T$ increases, electrons gain sufficient thermal energy to overcome the higher barriers, leading to a higher $q \varphi_b$ extracted from $I$-$V$ characteristics.

Capacitance-voltage ($C$-$V$) measurements were performed from 300 K to 600 K. Based on the linear extrapolation of the $1/C^2$-$V$ data, $V_{bi}$ and $N_D - N_A$ can be extracted.\textsuperscript{20} Figure 2(c) shows the extracted $V_{bi}$ and $N_D - N_A$ at 300–600 K. $V_{bi}$ shows a similar value compared to that extracted from the $I$-$V$ characteristics. It decreases with the increasing $T$, agreeing with other reports in the literature.\textsuperscript{20} The changes in $N_D - N_A$ in the drift region are very minimal as a function of $T$, indicating that most of the donors and acceptors have been fully ionized in the room temperature.

Figure 2(d) shows the forward $I$-$V$-$T$ characteristics plotted in the linear scale, and Fig. 2(e) shows the extracted differential specific $R_{in}$. The $R_{in}$ increases from $\sim$8.5 m$\Omega$ cm$^2$ to $\sim$13.5 m$\Omega$ cm$^2$ as $T$ increases from 300 K to 600 K, mainly due to the mobility degradation at higher $T$. At $T > 400$ K, the $R_{in}$ increases slowly with $T$, indicating the existence of a compensation mechanism that counters the impact of mobility degradation. From the backside circular transmission-line measurements, the Ohmic contact resistance was found to show little dependence on $T$. This indicates that the compensation is probably due to the increased donor ionization at high $T$. As $N_D - N_A$ in the drift region does not increase with $T$, the increased donor ionization is likely to occur in the n$^+$-Ga$_2$O$_3$ substrate. This could also explain the minimal increase\textsuperscript{20,21} or even reduction\textsuperscript{20,22} in the $R_{in}$ of vertical Ga$_2$O$_3$ SBDs at higher $T$ reported by other groups. The recently observed deep-level 110 meV unintentional donor in the Ga$_2$O$_3$ substrate possibly accounts for this increased ionization at high $T$.\textsuperscript{20}

Figure 3(a) shows the typical reverse $I$-$V$ characteristics of the fabricated vertical Ga$_2$O$_3$ SBDs at room temperature and the fitting based on the TE and variable-range-hopping (VRH) model. (b) Schematic illustration of TFE, VRH, and trap-assisted space-charge-limited conduction (SCLC) mechanisms. The solid blue line represents the TFE and VRH being in series. The dashed blue line represents the TFE to conduction band at 550 K and 600 K. (c) Reverse $I$-$V$ characteristics at 400–600 K up to 500 V and the fitting based on the TFE model. (b) Reverse current density ($J$) vs the peak E-field at the Schottky contact in a semilog plot at 400, 450, and 500 K. (d) In ($J$) vs $T^{-1.25}$ for the $J$ extracted at the reverse biases of 400, 450, and 500 V.

$$J_{TFE} = \frac{A^* T q h E}{2\pi} \sqrt{\frac{\pi}{2 m^* k T}} \times \exp \left( -\frac{q}{k T} \left( \varphi_b - \Delta \varphi_{\text{H},0} - \frac{q (h E)^2}{24 m^* (2\pi k T)} \right) \right),$$

(3)

where $E$ and $m^*$ are Planck’s constant and the electron effective mass in Ga$_2$O$_3$, respectively. $E$ and $\Delta \varphi_{\text{H},0}$ are the E-field at the Schottky

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contact at the reverse bias $V$ and the barrier lowering at zero reverse bias, respectively, which are given by \(^{(4)}\)

$$E = \sqrt{2q(N_D - N_A)(V_{bi} - V)/\varepsilon,}$$

$$\Delta \varphi_{bd} = \frac{1}{2}(N_D - N_A)V_{bi}/8q\sigma^2\varepsilon^2,$$  \((5)\)

where $\varepsilon$ is the electric permittivity of Ga$_2$O$_3$. The $N_D - N_A$ and $V_{bi}$ extracted from C-V measurements are used here.

At the reverse bias above 100 V, the leakage current exhibits a $\ln(I) \propto V$ relation. This indicates that the leakage current starts to be limited by the electron transport in the depletion region and the dominant leakage mechanism to be the electron variable-range-hopping (VRH) through defect-related states (dislocation or traps).\(^{(29,30)}\) This mechanism can be depicted by electron hopping via a localized “defect mini-band,” as shown in Fig. 3(b). A similar VRH through threading dislocations has been identified to be a major leakage mechanism in vertical GaN power SBDs\(^{(1)}\) and PN diodes.\(^{(25,26)}\) It is worth mentioning that, at lower reverse bias (<100 V), the $q\varphi_{bd}$ in the TFE model that provides the best fit to experimental data, 0.95 eV, is lower than the Schottky barrier height extracted from forward I-V characteristics (~1.2 eV). This indicates that most of the electrons were injected into the defect mini-band rather than the conduction band.

When the reverse bias is above ~500 V, the leakage current becomes higher than the VRH fitting. With an accumulated amount of electrons trapped in the depletion region, the current gradually becomes limited by space charge conduction. This trap-assisted space-charge-limited conduction (SCLC) mechanism is supported by a $I \propto V^4$ relation.\(^{(31)}\) This leakage mechanism has also been observed in vertical GaN power SBDs,\(^{(32)}\) PN diodes,\(^{(33,34)}\) and FinFETs.\(^{(35)}\) The device ultimate breakdown is destructive and occurs at the device edge, which is limited by the peak E-field in the FP oxide.\(^{(12)}\)

To study the high-temperature leakage mechanisms of our Ga$_2$O$_3$ SBDs, I-V measurements were performed up to a reverse bias of 500 V up to 600 K. Figure 3(c) shows the experimental reverse I-V-T characteristics from 400 K to 600 K and the fitted curves based on the TFE model. At 400 K and 450 K, the leakage current shows TFE-like behaviors at the reverse biases below 300 V, indicating that it is limited by the source of electrons, and then deviates toward the bulk semiconductor limited mechanism at high biases. The fitted energy barrier is getting closer to the Schottky barrier height at higher $T$, indicating an increased injection into the conduction band compared to the injection into the defect mini-band. When $T$ increases further (550 K and 600 K), the TFE model agrees with the device leakage over the entire voltage range and the fitted energy barrier is almost identical to the Schottky barrier height extracted from forward I-V-T characteristics. This indicates that the leakage is dominated by the TFE to conduction band.

To verify if VRH dominates the high-voltage leakage at 300–500 K, we investigated the dependence of the leakage current on both the E-field and $T$. The field- and $T$-dependence of the VRH current is described by\(^{(29,36)}\)

$$J_{VRH} = J_0 \exp \left( \frac{eEa}{2kT} \left( \frac{T_0}{T} \right)^{1/4} \right),$$  \((6)\)

where $J_0$ is the low-field current density, $T_0$ is a characteristic temperature parameter, $C$ is a constant, and $a$ is the localization radius of the electron wave function. Figure 3(d) plots the $\ln(J)$ vs the peak E-field in the depletion region calculated by \(^{(4)}\), which shows a good linear dependence when the peak E-field is above 1 MV/cm (corresponding to the reverse voltage over ~300 V). Figure 3(e) plots the $\ln(J)$ vs $T^{-1.25}$ at the reverse biases of 400–500 V, which shows good linear dependence. These results validate the VRH mechanism at high reverse voltages at 300–500 K.

To further understand the impacts of biases and temperatures on the leakage limitation by either the source of electrons or their bulk transport, we look at the VRH drift velocity ($v_d$), which can be modeled using a Gaussian disorder model,\(^{(9,39)}\)

$$v_d = \mu E \approx \frac{v_0 b}{2} \exp \left( -\frac{\sigma^2}{(kT)^2} \right) \left[ \exp \left( \frac{qCe}{kT} \right) - 1 \right],$$  \((7)\)

where $v_0$ is the hopping frequency, $b$ is the average trap-to-trap distance, $\sigma$ is the energy sigma, and $E$ is the electric field. From \((7)\), a higher temperature will lead to an increased $v_d$ at the same E-field (bias) and therefore, a smaller transit time in the depletion region. This suggests that the leakage current can be less limited by the bulk transport at the same voltage. As a result, the characteristic voltage, at which the TFE-like electron-source limited current transitions into the VRH-like bulk-limited current, increases with temperature. This agrees well with the experiment, as this characteristic voltage increases from ~100 V at 300 K to ~270 V at 400 K. At even higher $T$, the transient time is even smaller, and electrons are less localized at the defect mini-band. As a result, the TFE to conduction band dominates the leakage.

Figure 4 compares the maximum operational temperature vs the maximum reverse bias reported for the Ga$_2$O$_3$,\(^{(15,20,27,40)}\) GaN,\(^{(11,41)}\) and SiC\(^{42,43}\) based Schottky barrier power rectifiers. Our work presents the best combination of high-voltage and high-temperature performance in Ga$_2$O$_3$ power diodes and our highest operating temperature exceeds the ones reported for GaN and SiC SBDs with a similar operation voltage. When $T$ increases from 300 K to 500 K, the leakage current of our Ga$_2$O$_3$ SBDs only increases by about tenfold at 500 V, while at least 100-fold leakage increase at 500 V is shown in vertical GaN\(^{(31,41)}\) and SiC\(^{42}\) SBDs with a similar BV. It is also worth mentioning that the

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**FIG. 4.** The maximum operational temperature vs the maximum reverse bias reported for Ga$_2$O$_3$, GaN, and SiC based Schottky barrier power rectifiers.
high-temperature GaN and SiC SBDs typically have more complicated device designs, such as trench metal-oxide-semiconductor barrier Schottky (TMBS) or junction barrier Schottky (JBS) structures, while our Ga$_2$O$_3$ SBDs use a much simpler edge termination. These comparisons show the great potential of Ga$_2$O$_3$ SBDs for high-temperature and high-voltage power applications.

In summary, this work presents the high-temperature forward and reverse characteristics of the high-voltage vertical Ga$_2$O$_3$ SBDs and high-voltage power applications.

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